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Multifunctional Fluid Power Components using Engineered Lattice Structures

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Overview

- > Introduction
- Multifunctional Unit Cells
- Determining Effective Thermal Conductivities
- Developing Thermal-Management Structure
- > Experimental Results
- Next Steps
- Conclusions

Multifunctional Structure

- > Heat dissipation
- ➤ Load bearing
- > Reduced dead weight
- > Potential to reduce noise & vibration

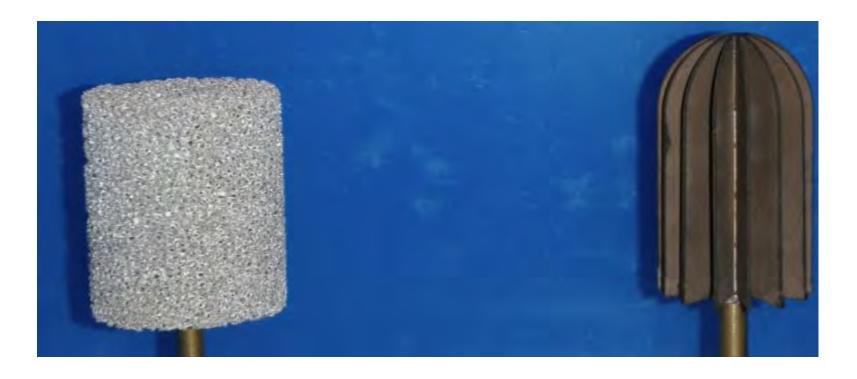
State-of-the-art

Metal Foam

- Multifunctional capabilities
- Not optimized

Finned Heat Structure

- Not multifunctional
- Not optimized



Ex.: Powered Personal Devices

- Safety considerations of heat
 - Burn
 - Pain
 - "Toasting"
- Discomfort issues

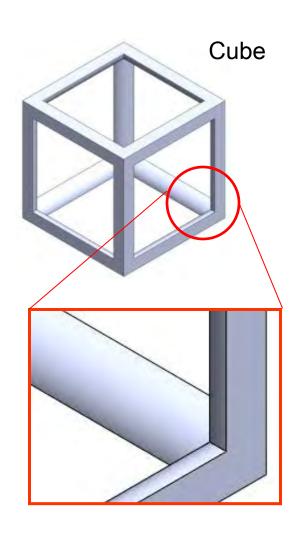




Multi-Institutional Patent Pending

CCEFP Project 2D & Test Bed 6 - Concept Models:
Belt-worn or Orthosis-integrated Power Source

Multifunctional Unit Cells



- Thermal conductivity as a function of strut diameter and cell size
- Varied strut diameters; 0.2L, 0.5L, and 0.8L
- Initial cell size 1 inch, later scaled to determine size effects
- Analyzed Cube, Ultra Cube, and Super Cube configurations

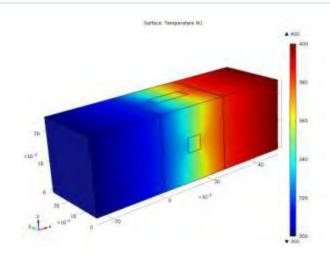








Modeling the Cubes



$$q^{\prime\prime} = \frac{\Delta T}{R_{equiv}}$$

$$K = \frac{x}{A(\frac{\Delta T}{q''} - 2R_{cop})}$$

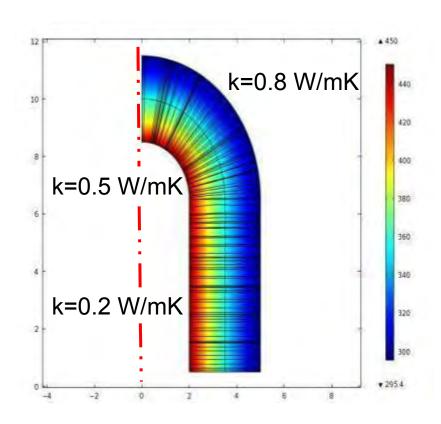
- Stagnant air (no convection)
- Base material aluminum (k=160 W/mK)
- Solved for three orthogonal directions
- Boundary conditions
 - T1=400K
 - T2=300K
 - Other four sides insulated

Model Results

- Determined the bulk thermal conductivity of three lattice structures in the three orthogonal directions
- Heat flux scaled linearly to length of cell, resulting in a constant conductivity
- Analyzed structures with varying material, scaling equations based on thermal conductivity
- Investigated the effects of internal convection negligible
- Working to determine the energy balance via mass transfer through the structure

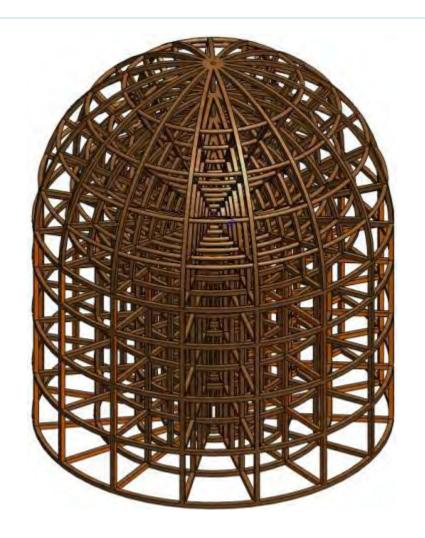
Optimizing K_{eff}

- Specified inner temperature
- Free external convection on outer surface
- ➤ Target: 45°C surface temp with "radial" heat flux



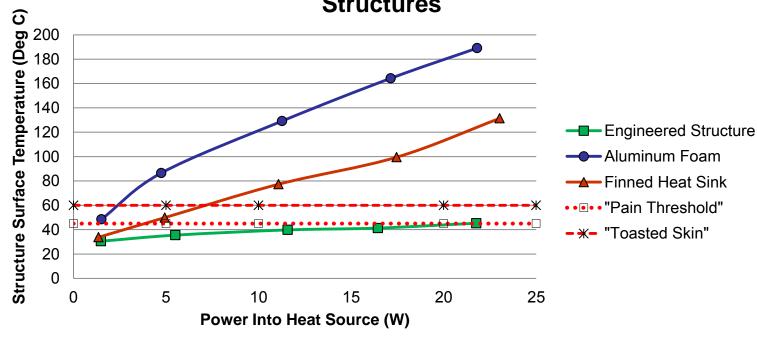
Developing the Structure

- Geometric relationships derived to maintain "squareness"
- Matlab® script calculates divisions and strut lengths
- Iterate to meet minimum feature size (secondary structure optimization)



Experimental Results

Experiment: Comparison of Thermal-Management Structures



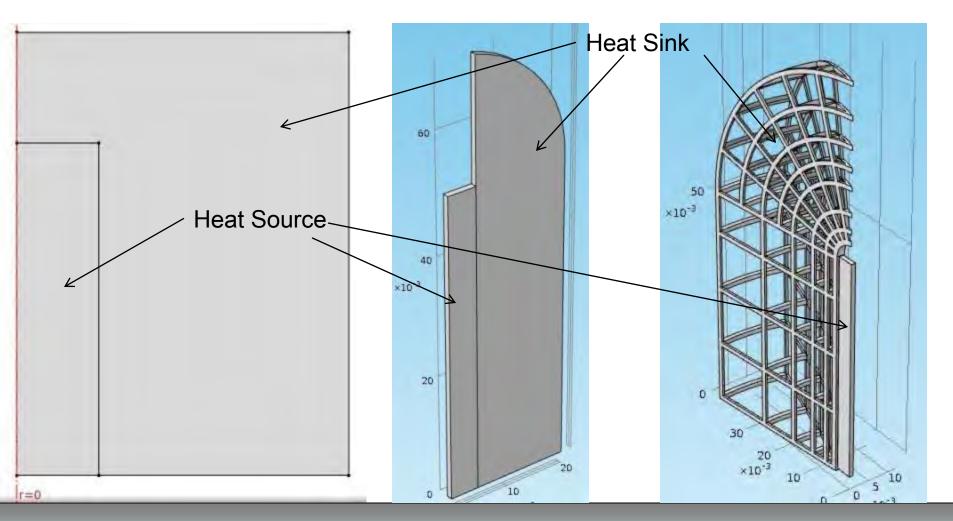
2

0-05 -0.5 0

- > Same mass
- > Same material
- ➤ Structure area = 2(fin area)

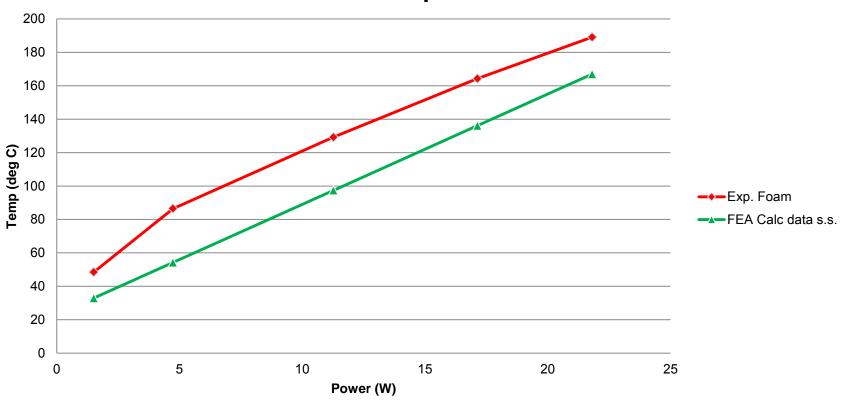
- ➤ Both cast
 - Cu/Al alloy
 - 43W/mK

Model Setup



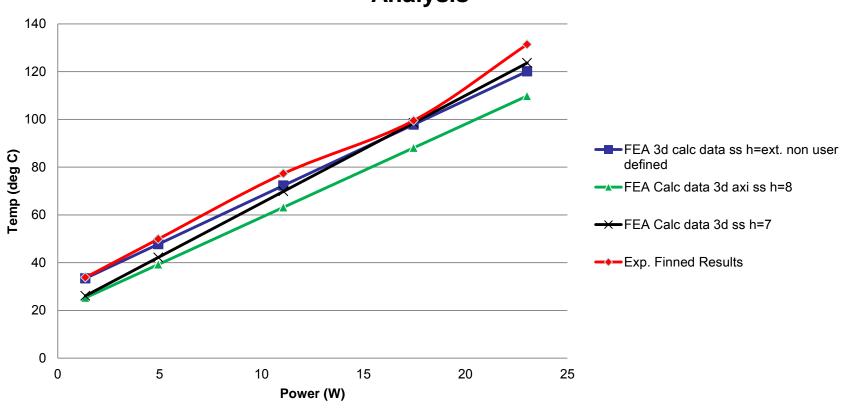
Metal Foam Comparison

Comparison of Linearly Derived Equations of Foam FEA to Exp.



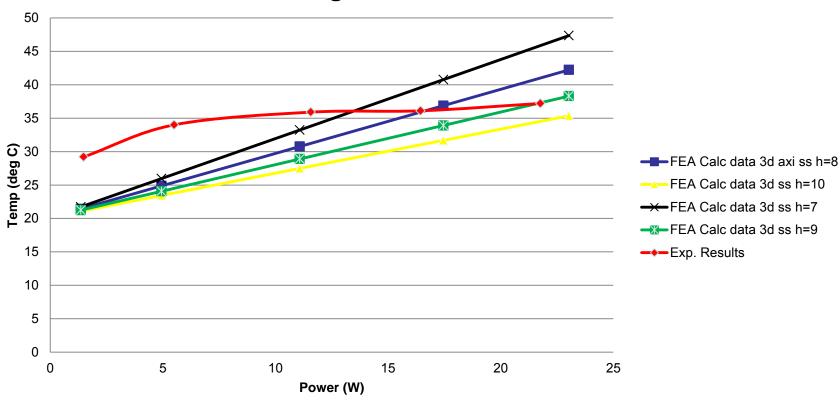
Finned Heat Sink Comparison

3D Single Fin Comparison of Measured Data and FEA Analysis



Engineered Structure Comparison

Comparison of FEA and Exp. Derived Equations for Engineered Structure



Next Steps

- Design & fabrication of multi-functional orthosis structure
- Continue multi-functional characterizations
- > Determine if second-order relations are best
- Continue development of the structure-sizing relations
- Continue development of automated free-form algorithms

Conclusions

- Passive thermal management can be achieved through the design of components using engineered lattices
- Target performance can be attained by varying material and geometry
- > Benefits
 - Integrated, minimal-mass, multifunctional design, e.g. load bearing and thermal management

Acknowledgements

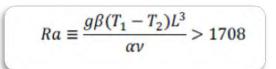
- CCEFP
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- MSOE faculty
- Past, and present, assistants, REU's & RET's

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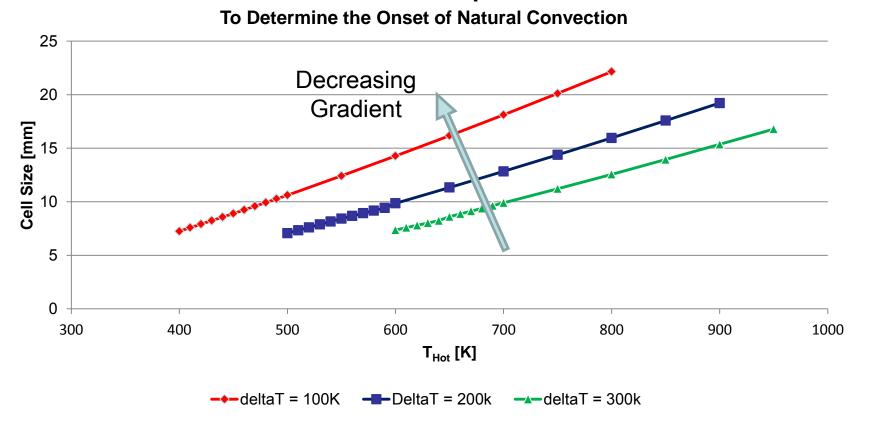
Thank you!

Questions?

Onset of Convection



Cell Size vs. Temperature



Geom.-Dependent Keff

Simple Cube

```
Kxx(x,y,z) = 7.098\emptyset x^2 + 24.463\emptyset y^2 + 24.484\emptyset z^2 + 33.195\emptyset x\emptyset y + 33.204\emptyset x\emptyset z  + 7.391\emptyset y\emptyset z + 54.746\emptyset x - 25.441\emptyset y - 25.465\emptyset z Kyy(x,y,z) = 24.491\emptyset x^2 + 7.094\emptyset y^2 + 24.473\emptyset z^2 + 33.190\emptyset x\emptyset y + 7.380\emptyset x\emptyset z  + 33.181\emptyset y\emptyset z - 25.463\emptyset x + 54.755\emptyset y - 25.443\emptyset z Kzz(x,y,z) = 36.417\emptyset x^2 + 36.373\emptyset y^2 + 77.304\emptyset z^2 - 24.288\emptyset x\emptyset y + 28.356\emptyset x\emptyset z  + 28.318\emptyset y\emptyset z - 20.033\emptyset x - 19.977\emptyset y + 28.343\emptyset z
```

Ultra Cube

```
Kxx(x,y,z) = 232.076\emptyset x^2 + 176.753\emptyset y^2 + 176.7531\emptyset z^2 - 205.439\emptyset x\emptyset y - 205.437\emptyset x\emptyset z - 120.536\emptyset y\emptyset z + 26.394\emptyset x + 37.753\emptyset y + 37.747\emptyset z
Kyy(x,y,z) = 176.760\emptyset x^2 + 232.100\emptyset y^2 + 176.751\emptyset z^2 - 205.453\emptyset x\emptyset y - 120.55\emptyset x\emptyset z - 205.456\emptyset y\emptyset z + 37.750\emptyset x + 26.383y + 37.761\emptyset z
Kzz(x,y,z) = 176.755\emptyset x^2 + 176.755\emptyset y^2 + 232.100\emptyset z^2 - 120.556\emptyset x\emptyset y - 205.462\emptyset x\emptyset z - 205.457\emptyset y\emptyset z + 37.750\emptyset x + 37.757\emptyset y + 26.386\emptyset z
```

Super Cube

```
\begin{split} Kxx(x,y,z) &= 198.514\emptyset x^2 + 232.055\emptyset y^2 + 228.267\emptyset z^2 - 183.149\emptyset x\emptyset y - 186.909\emptyset x\emptyset z \\ &- 206.603\emptyset y\emptyset z + 50.686\emptyset x + 19.065\emptyset y + 25.510\emptyset z \\ Kyy(x,y,z) &= 231.324\emptyset x^2 + 197.766\emptyset y^2 + 231.324\emptyset z^2 - 185.432\emptyset x\emptyset y - 205.144\emptyset x\emptyset z \\ &- 185.432\emptyset y\emptyset z + 20.690\emptyset x + 52.332\emptyset y + 20.690\emptyset z \\ Kzz(x,y,z) &= 229.014\emptyset x^2 + 229.031\emptyset y^2 + 199.260\emptyset z^2 - 208.119\emptyset x\emptyset y - 184.677\emptyset x\emptyset z \\ &- 184.664\emptyset y\emptyset z + 23.892\emptyset x + 23.871\emptyset y + 49.069\emptyset z \end{split}
```