

Multiphysics Simulation of the Effect of Sensing and Spacer Layers on SAW Velocity

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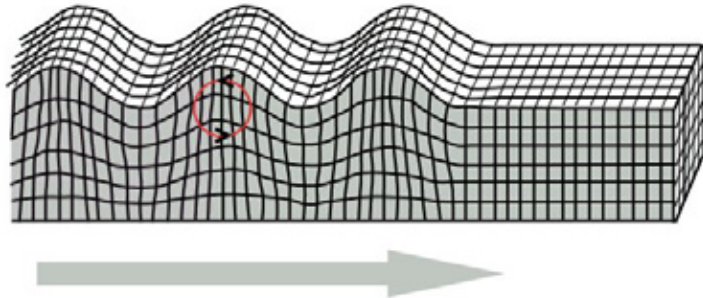
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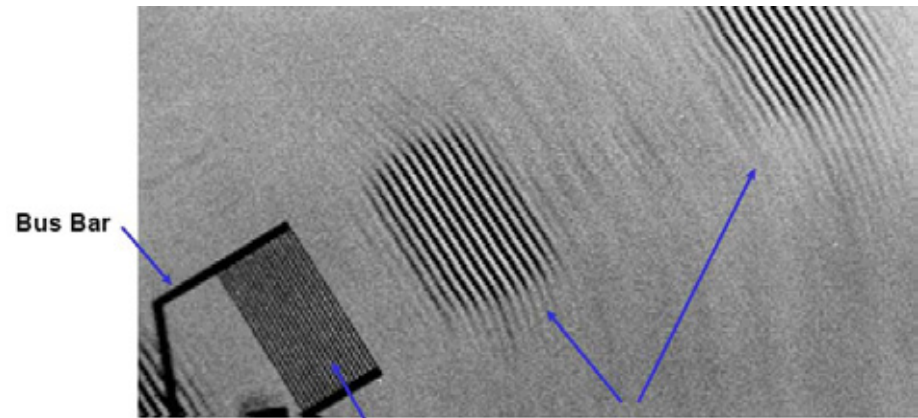


Surface Acoustic Wave (SAW) Sensor

Rayleigh Wave



Schematic of surface acoustic wave

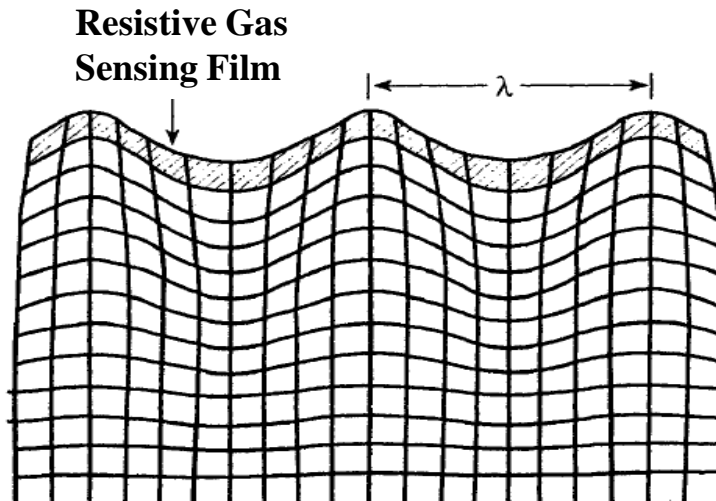


Interdigital Transducer, IDT Surface Acoustic Wave, SAW

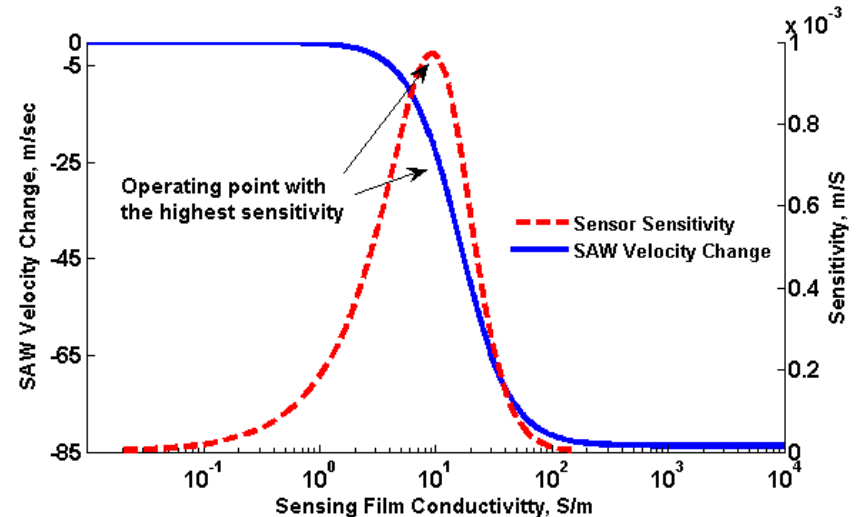
Rendl et al. UFFC 2002

- Surface acoustic wave: acoustic waves traveling along the surface of an elastic body, with an amplitude decays exponentially with depth
- SAW sensor: using interdigital transducer to detect surface acoustic wave velocity change caused by surface perturbation
-- *Surface conductivity change on piezoelectric substrate*
- Research interest: SAW oxygen sensor in combustion process (up to 1000 C)

Conductivity Based SAW Gas Sensor



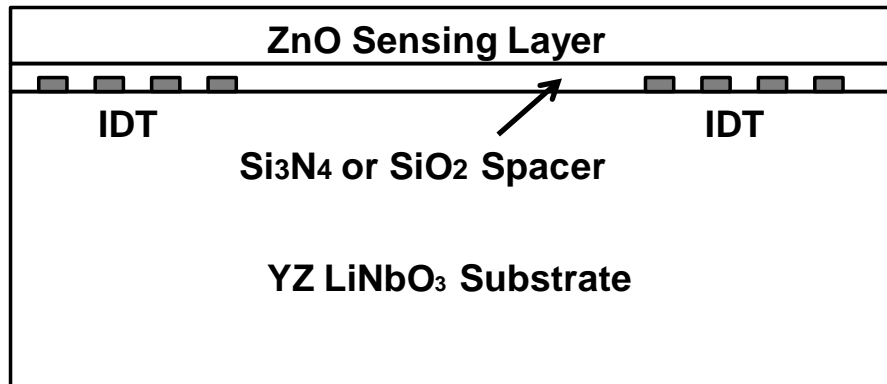
Acoustic Wave Sensor: Theory, Design, and Physico-Chemical Applications / Ballantine



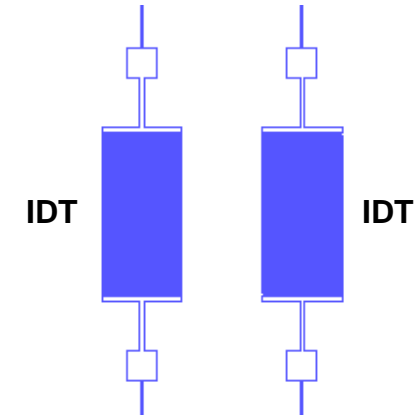
Calculated surface acoustic wave velocity and sensitivity as a function of surface sensing film conductivity

- Conductivity based SAW gas sensor concept: A resistive gas sensing layer on piezoelectric substrate surface
- Analytic theory excludes the mechanical effect of sensing and spacer layer
- Accurate multiphysics finite element simulation is needed to include both the electrostatic effect and mechanical effect of sensing and spacer layer

Proposed SAW Sensor Structure



Side View of SAW sensor



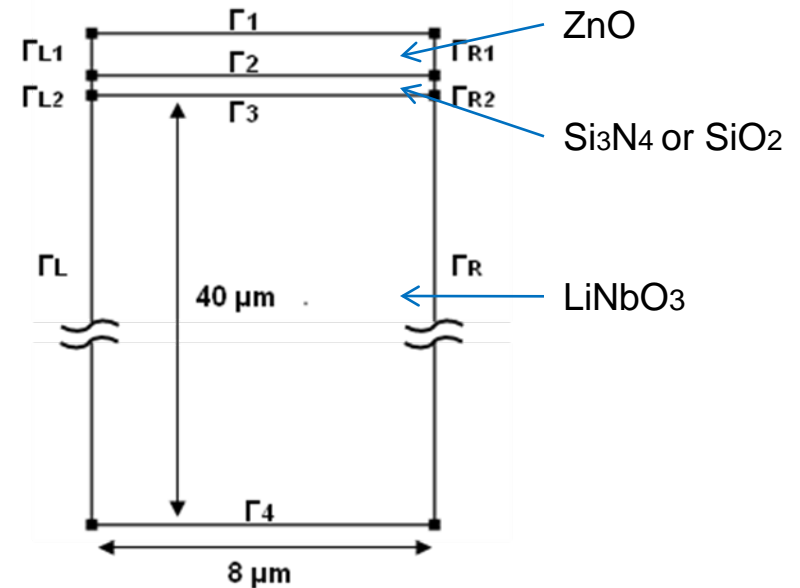
L-edit pattern of SAW sensor

- SAW gas sensor structure
 - Oxygen surface sensing layer: ZnO;
 - Spacer layer: Si₃N₄ or SiO₂;
 - Piezoelectric substrate: YZ cut LiNbO₃;
 - Rayleigh surface acoustic wave wavelength: $\lambda=8 \mu\text{m}$
- Simulation objective
 - To analyze the effect of thickness and materials of sensing and spacer layer on sensor sensitivity
 - To optimize the design of SAW oxygen sensor used in combustion process

Simulation Setup

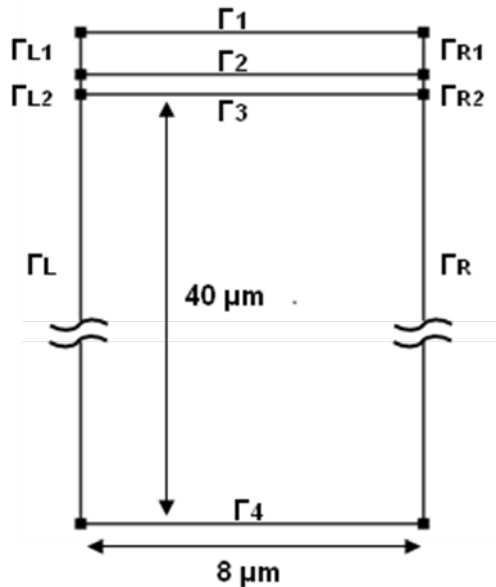
	Mechanical BC	Electrical BC
Γ_1	Free	zero charge /symmetry
Γ_2, Γ_2	Free	Continuity
Γ_4	Fixed	Ground
$\Gamma_R, \Gamma_{R1}, \Gamma_{R2}, \Gamma_L, \Gamma_{L1}, \Gamma_{L2}$	Periodical boundary conditions	

Simulation Boundary Condition



- Eigenfrequency analysis in multiphysics finite element package COMSOL 3.4a 2D piezo plane strain mode (smppn)
- Periodic boundary condition to simulate the surface acoustic wave propagation
- Surface acoustic wave velocity = Eigenfrequency \times Width

Simulation Setup



$$\text{Continuity Equation } \nabla \cdot \vec{J} = -\frac{\partial \rho_v}{\partial t} = j\omega \rho_v \quad \left. \vphantom{\nabla \cdot \vec{J}} \right\}$$

$$\text{Ohm's Law } \nabla \cdot \vec{J} = \nabla \cdot \sigma \vec{E} = \nabla \cdot (\sigma \epsilon_0 \epsilon_r \nabla V) \quad \left. \vphantom{\nabla \cdot \vec{J}} \right\}$$

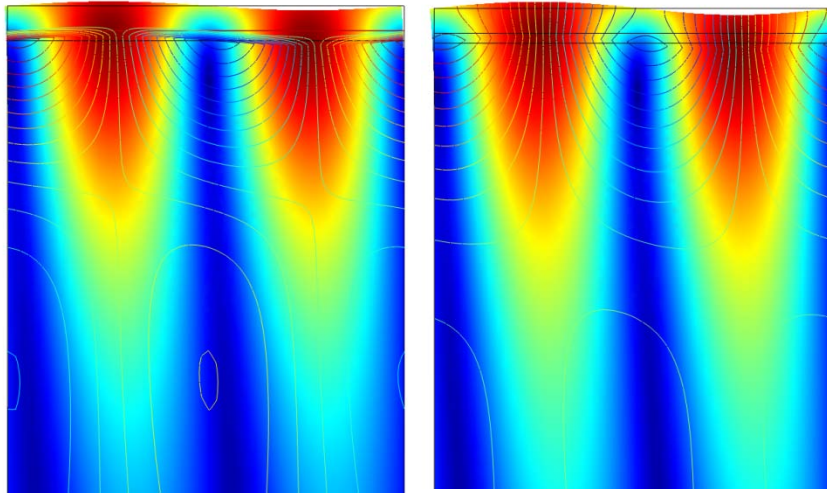
$$\Rightarrow \nabla \cdot (\sigma \epsilon_0 \epsilon_r \nabla V) = -j\omega \rho_v \quad \left. \vphantom{\nabla \cdot (\sigma \epsilon_0 \epsilon_r \nabla V)} \right\}$$

$$\text{Electrostatic Equation } -\nabla \cdot (\epsilon_0 \epsilon_r \nabla V) = \rho_v \quad \left. \vphantom{-\nabla \cdot (\epsilon_0 \epsilon_r \nabla V)} \right\}$$

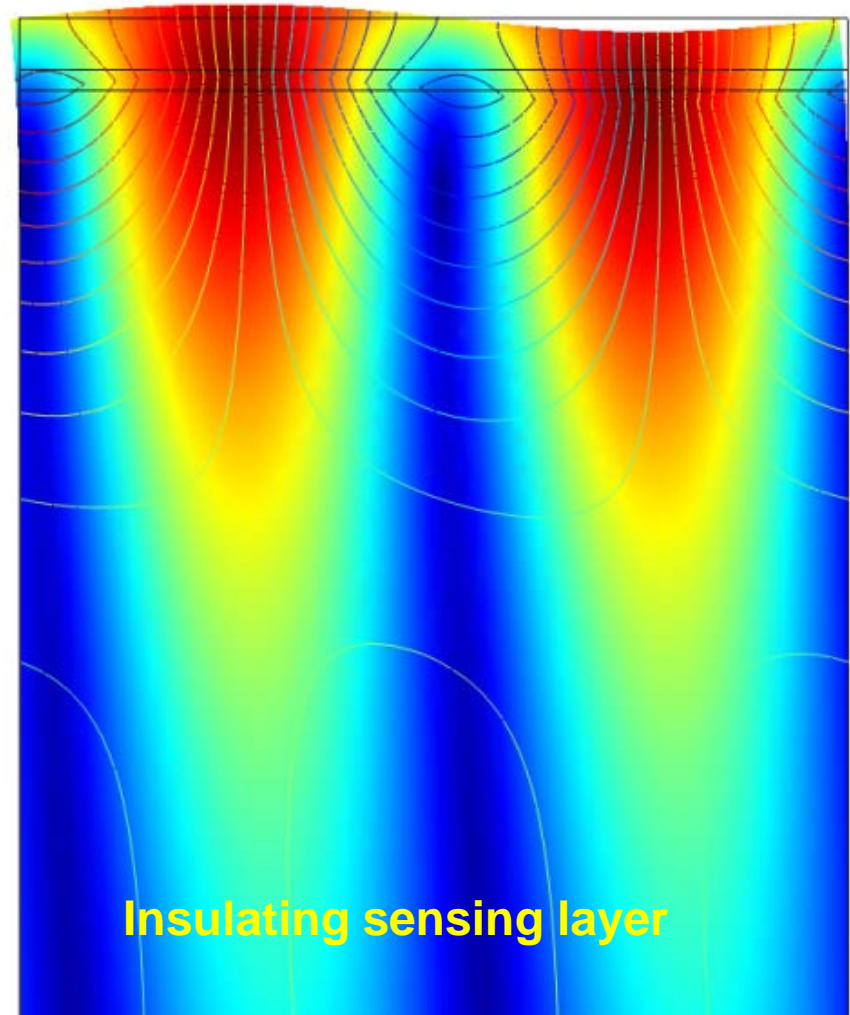
$$\Rightarrow -\nabla \cdot \left(\left(\frac{\sigma}{j\omega} + \epsilon_0 \epsilon_r \right) \nabla V \right) = \rho_v$$

- Sensing layer: Isotropic materials mode, electric equation enabled
 - Electrostatic equation $-\nabla \cdot (\epsilon_0 \epsilon_r \nabla V) = \rho_v$; Elastic equation $\mathbf{T} = \mathbf{c}_E \mathbf{S}$
 - Complex dielectric permittivity $\epsilon_r - j\sigma/\omega\epsilon_0$ to simulate conductivity
- Spacer layer: Isotropic materials mode, electric equation enabled
- Substrate: Piezoelectric materials mode
 - Piezoelectric equation: $\mathbf{T} = \mathbf{c}_E \mathbf{S} - e^T \mathbf{E} \quad \mathbf{D} = e \mathbf{S} + \epsilon_S \mathbf{E}$

Simulation Result

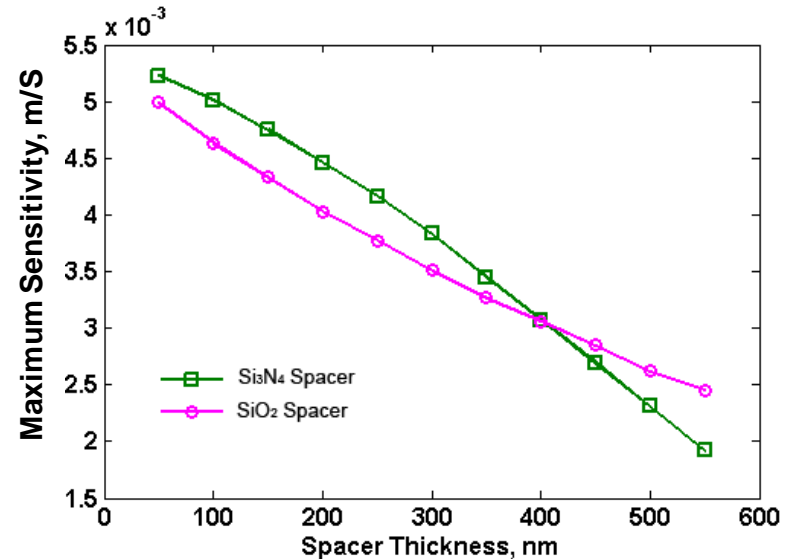
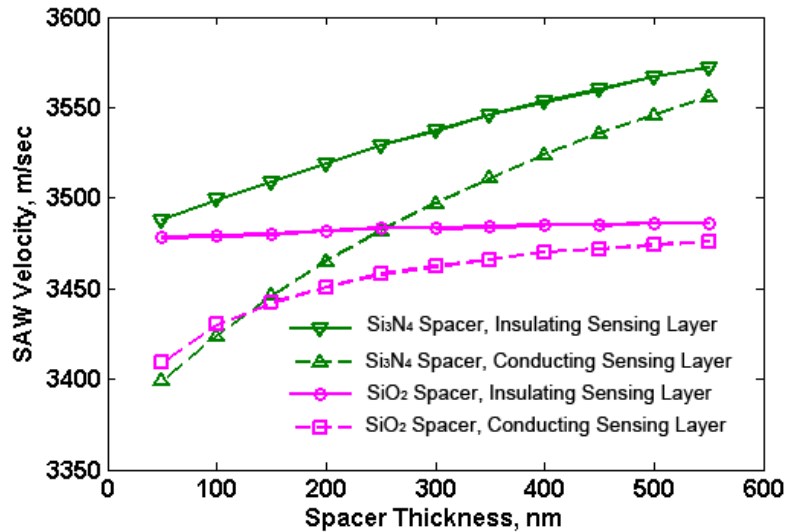


Conducting sensing layer Insulating sensing layer



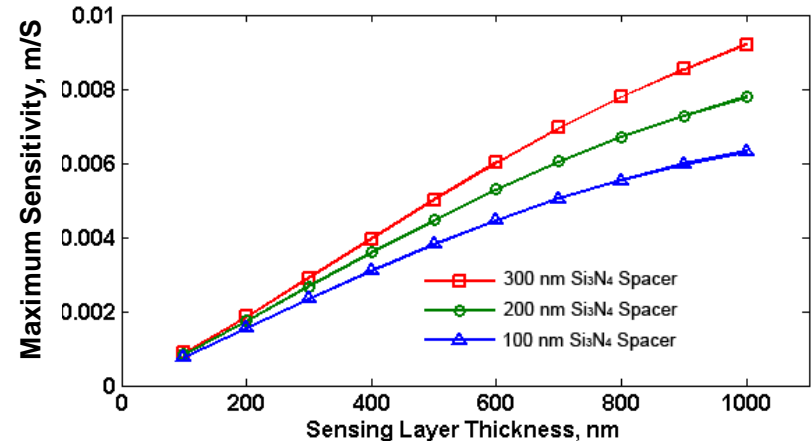
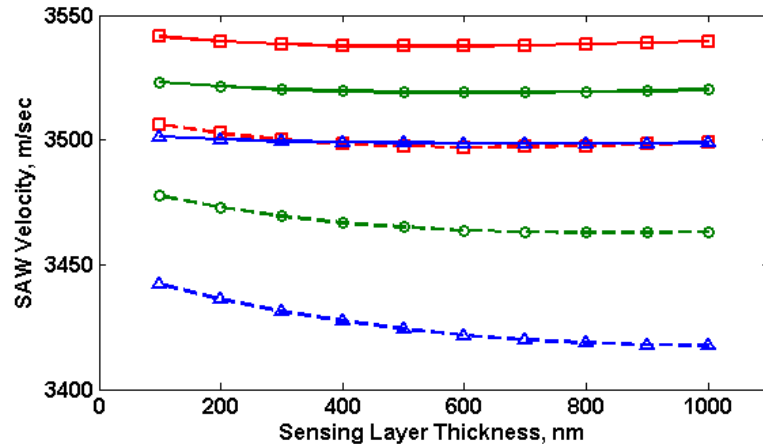
- Surface acoustic wave velocity change as a function of sensing layer bulk conductivity is simulated in different structure
- SAW sensor sensitivity is calculated by $S = -\frac{d(\Delta v/v_f)}{d\sigma_0}$

Effect of Spacing Layer



- $\text{ZnO}/\text{Si}_3\text{N}_4/\text{LiNbO}_3$ and $\text{ZnO}/\text{SiO}_2/\text{LiNbO}_3$ structures with different spacer thickness are simulated
- $\text{ZnO}/\text{Si}_3\text{N}_4/\text{LiNbO}_3$ structure has better sensitivity than $\text{ZnO}/\text{SiO}_2/\text{LiNbO}_3$ when the spacer is thinner than 400 nm
- The $\text{ZnO}/\text{Si}_3\text{N}_4/\text{LiNbO}_3$ structure is selected for the following simulation

Effect of Sensing Layer



- 300 nm Si₃N₄ Conducting
- 200 nm Si₃N₄ Conducting
- 300 nm Si₃N₄ Insulating
- △— 100 nm Si₃N₄ Insulating
- 200 nm Si₃N₄ Conducting
- △— 100 nm Si₃N₄ Conducting

- ZnO/Si₃N₄/LiNbO₃ structure with different sensing layer thickness are simulated
- The maximum sensitivity increase linearly as sensing layer thickness increase
- Thicker sensing layer has larger film conductivity change $\sigma_{film} = \sigma_{bulk} t$ resulting a higher sensitivity

Summary

- Surface acoustic wave propagation in $\text{ZnO}/\text{Si}_3\text{N}_4/\text{LiNbO}_3$ and $\text{ZnO}/\text{SiO}_2/\text{LiNbO}_3$ layered structures are simulated using COMSOL 3.4a 2D piezo plane strain mode.
- The effect of thickness and materials of sensing and spacer layer on the sensitivity are analyzed to optimize SAW gas sensor design
- The simulation result shows that the maximum sensitivity increase as the spacer gets thinner or the sensing layer gets thicker for both layered structure
- $\text{ZnO}/\text{Si}_3\text{N}_4/\text{LiNbO}_3$ layered structure shows higher sensitivity than the $\text{ZnO}/\text{SiO}_2/\text{LiNbO}_3$ layered structure with a spacer thickness ranges from 50 nm to 400 nm