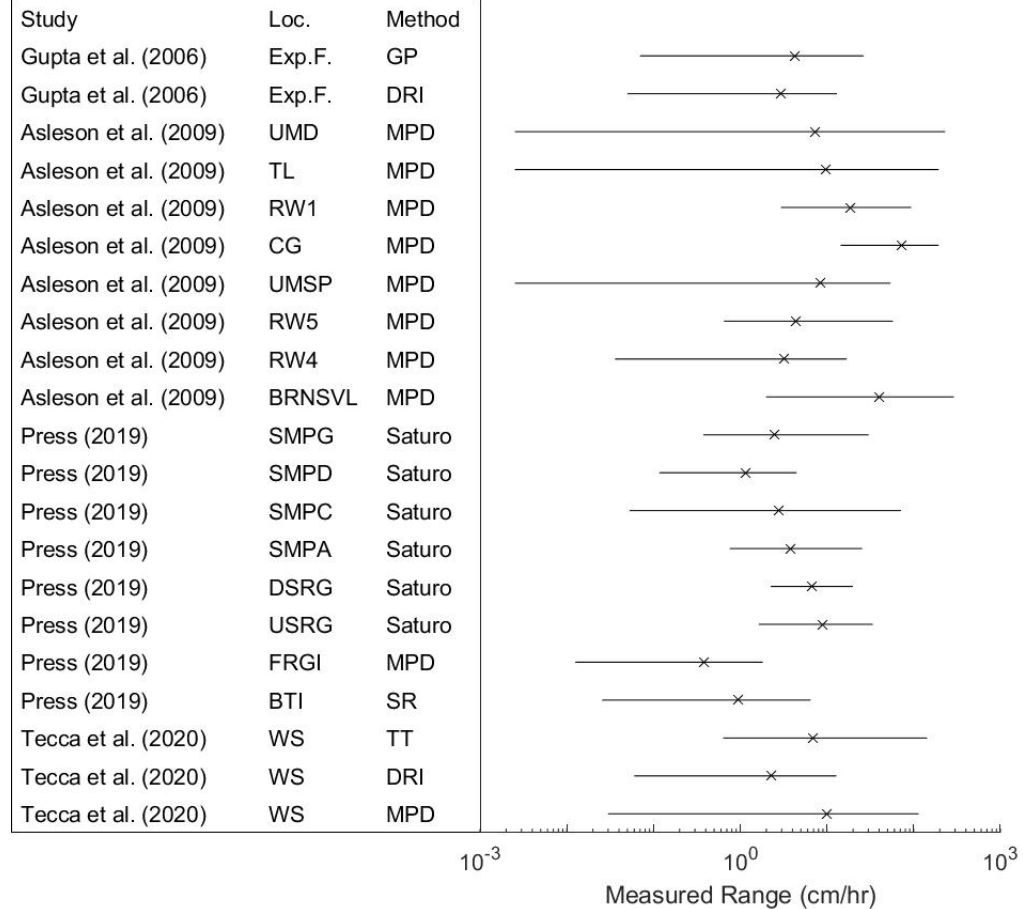


Precision and Bias in Field Methods for Measuring Soil Saturated Hydraulic Conductivity

Nicholas P. Tecca, John S. Gulliver, John L. Nieber



Variability in the Field

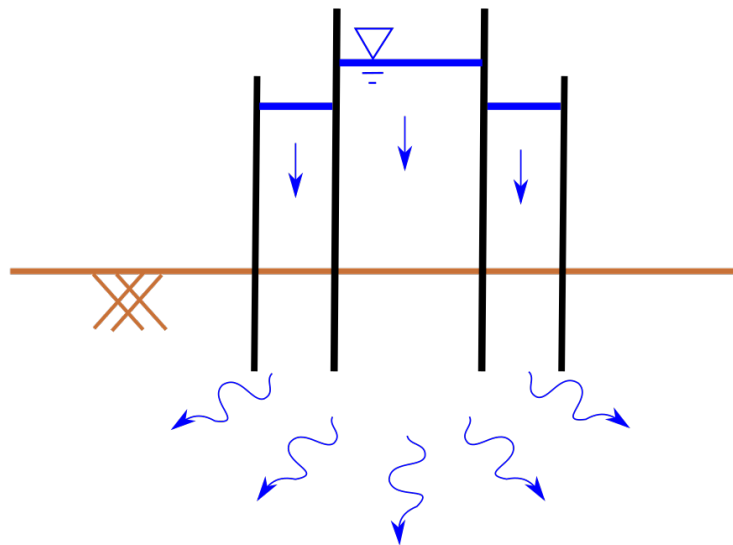


Objective

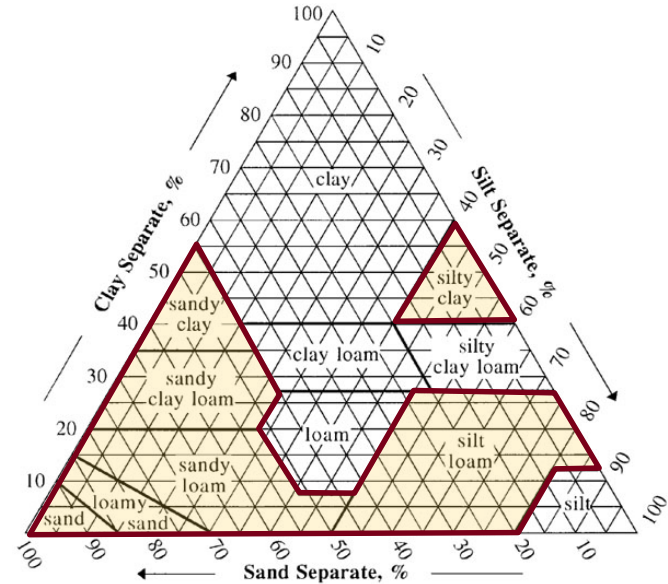
- Numerically estimate the accuracy (precision and bias) of infiltration measurement methods
 - 6 methods
 - 7 soil types
 - 5 antecedent soil moistures
 - Full factorial design
 - 210 simulations

Field Methods	Flow Condition		Dimensionality	
	Constant	Falling	1-D	3-D
Turf-Tec		X	X	
MPD		X		X
Saturo	X			X
Double Ring	X		X	
Well Permeameter	X			X
Pilot Infiltration Test	X		X	

Turf-Tec Infiltrrometer



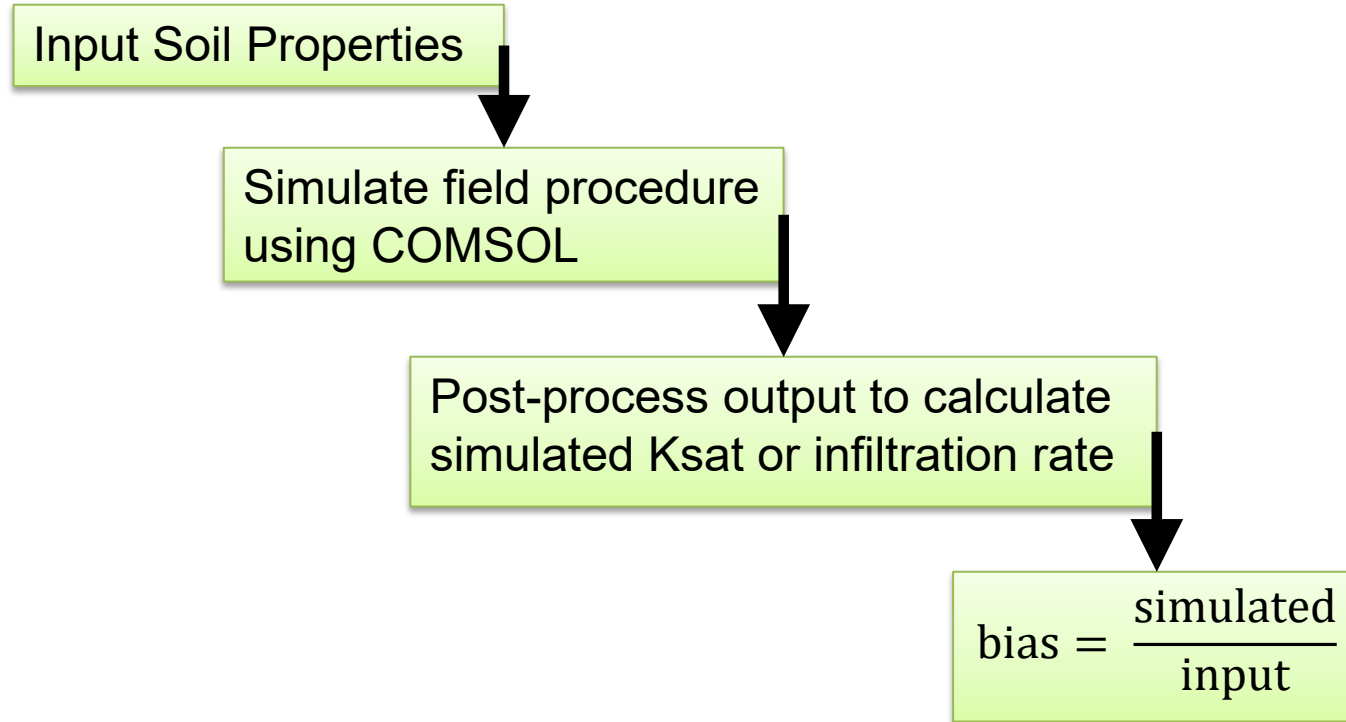
Simulated Soils



	Operating Range (in/hr)	SiC	SC	SiL	SCL	SL	LS	S	
		0.008	0.047	0.18	0.52	1.7	5.7	11.7	
TT	0.25 42								
MPD	0.098 590.6								
Sat.	0.0015 45.3								
DRI	0.014 14.2								
WP	0.014 141.7								
PIT	? 4								

Image Credits: USDA NRCS Soil Texture Calculator

Workflow

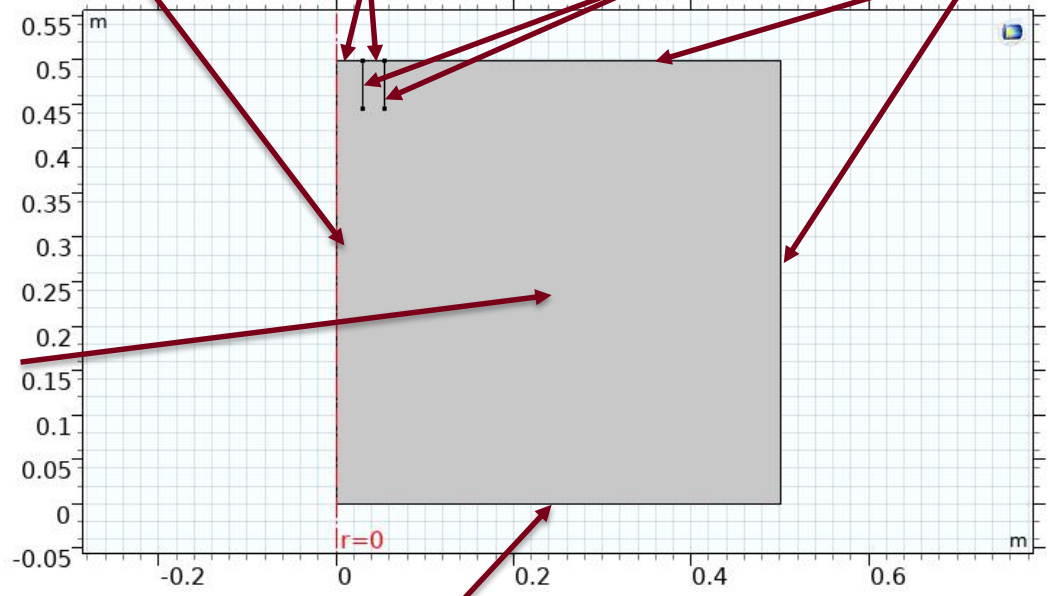


2-D Axisymmetric
Homogenous
Isotropic
Free-Draining

Pressure Head
Time-Variable
Interior Wall
No Flow

Axial Symmetry

Richards' Equation



$$\text{Mass Flux} = K_{\text{sat}} * dl.K_r * \rho$$

modified form of van Genuchten retention model

Effect of the shape of the soil hydraulic functions near saturation on
variably-saturated flow predictions

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Received 8 May 1998; received in revised form 10 June 2000; accepted 24 June 2000

Retention Model

Retention model:

User defined

Unsaturated condition:

un $\lfloor dl.Hp < hs$ 1

Liquid volume fraction:

θ $\lfloor \text{if}(dl.un, \text{thetar} + (\text{thetam} - \text{thetar}) / ((1 + \text{abs}(\text{VGalpha} * dl.Hp)^{\text{VGN}})^{\text{VGM}}), \text{thetas})$ 1

Effective saturation:

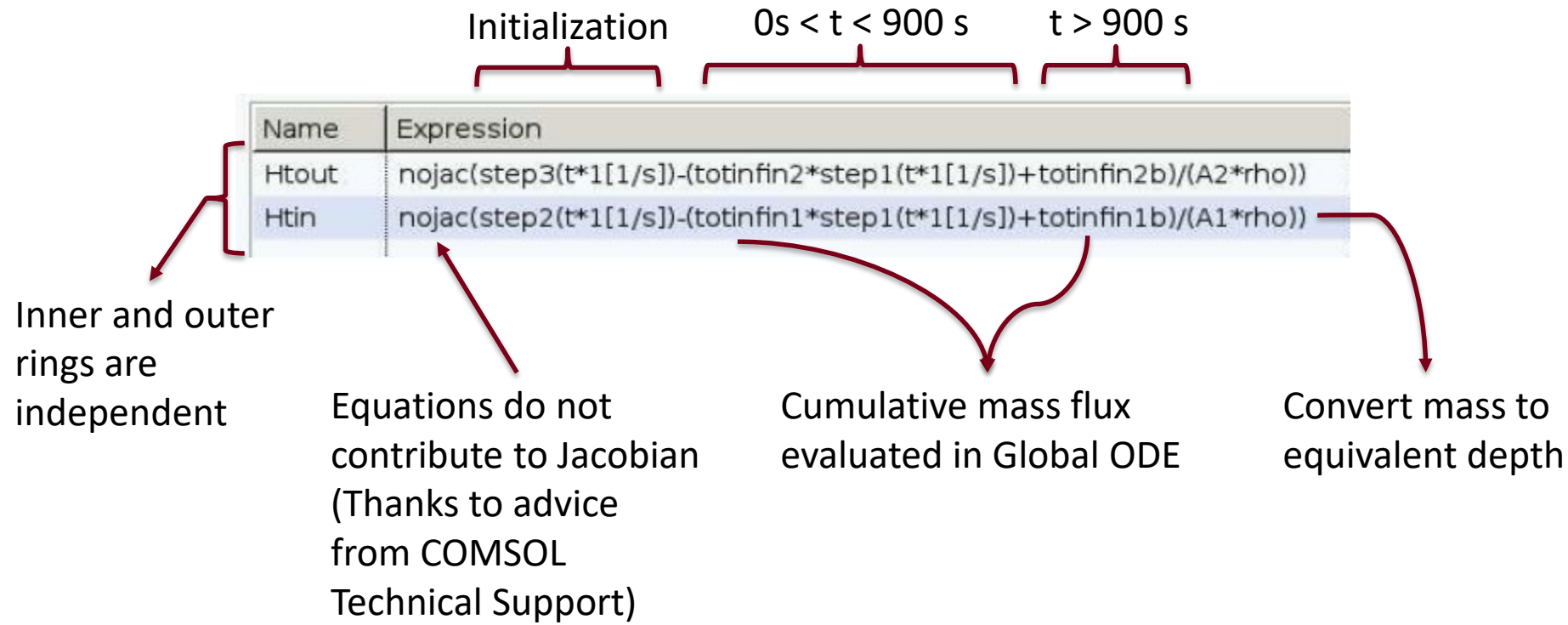
S_e $\lfloor \text{if}(dl.un, (dl.theta - \text{thetar}) / (\text{thetam} - \text{thetar}), 1)$ 1

Specific moisture capacity:

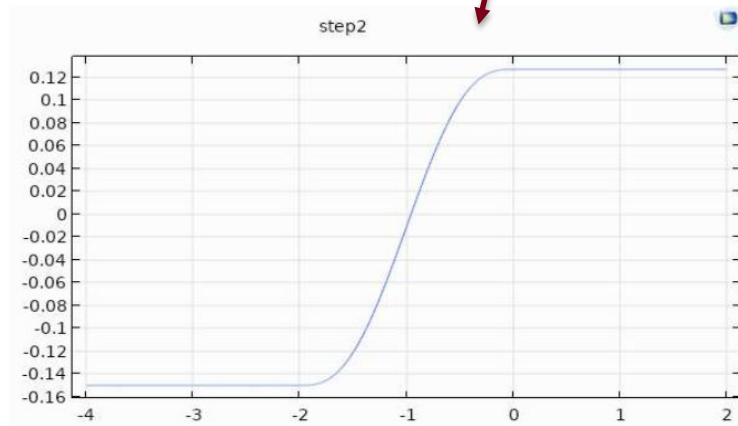
C_m $\lfloor \text{if}(dl.un, d(dl.theta, p) * \rho * dl.g, 0)$ 1/m

Relative permeability:

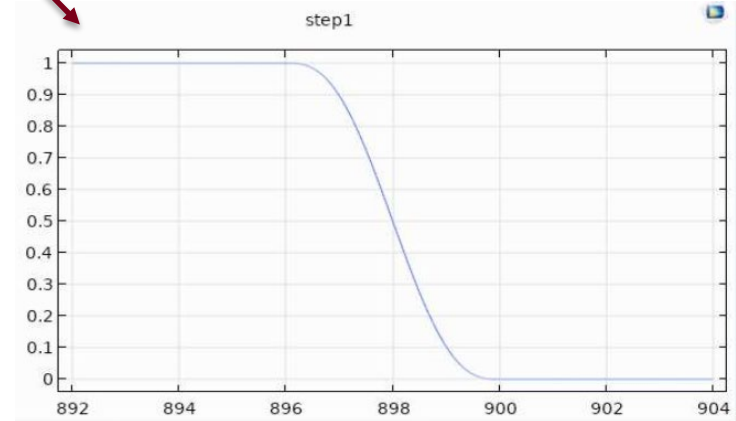
k_r $\lfloor \text{if}(dl.un, dl.Se^{0.5} * ((1 - FSe) / (1 - F1))^{2, 1})$ 1



Name	Expression
Htout	$\text{nojac}(\text{step3}(t*1[1/s])-(\text{totinfin2}*\text{step1}(t*1[1/s])+\text{totinfin2b}))/(\text{A2}*\text{rho})$
Htin	$\text{nojac}(\text{step2}(t*1[1/s])-(\text{totinfin1}*\text{step1}(t*1[1/s])+\text{totinfin1b}))/(\text{A1}*\text{rho})$

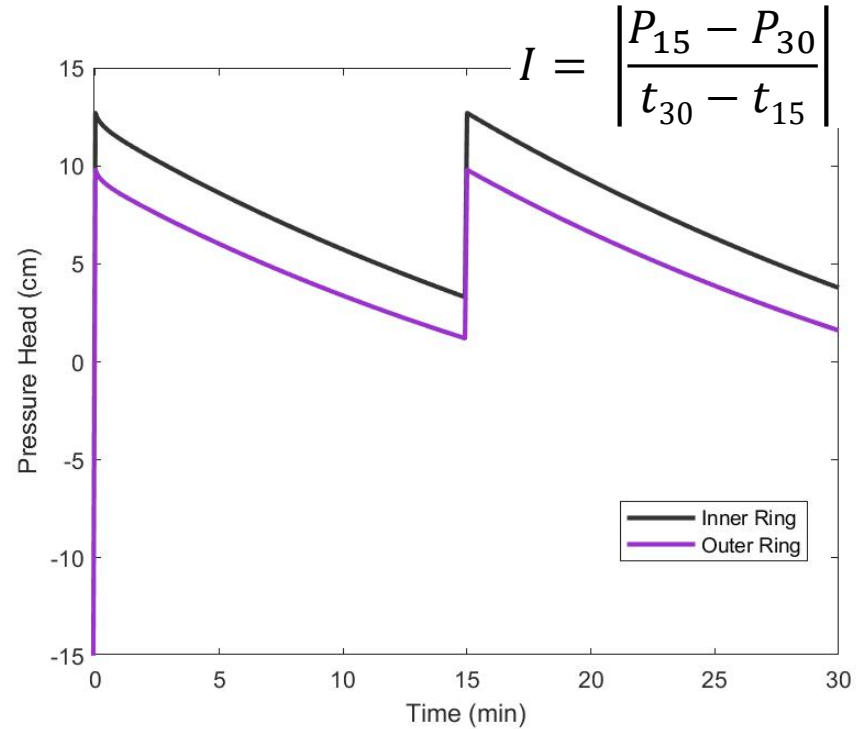
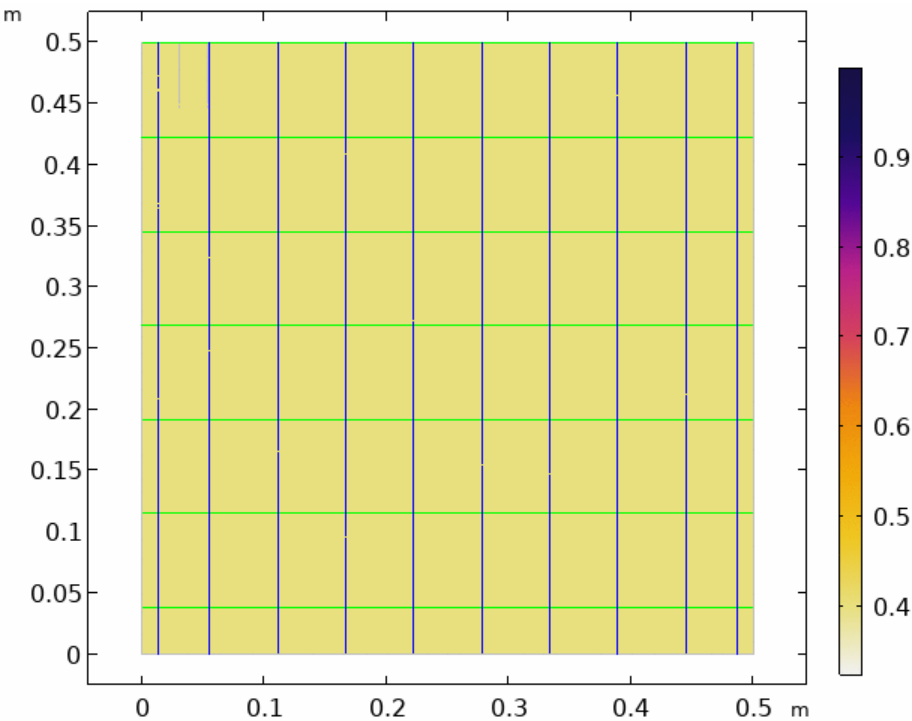


Initial filling of rings at t = 0 sec



Refilling rings at t = 900 sec

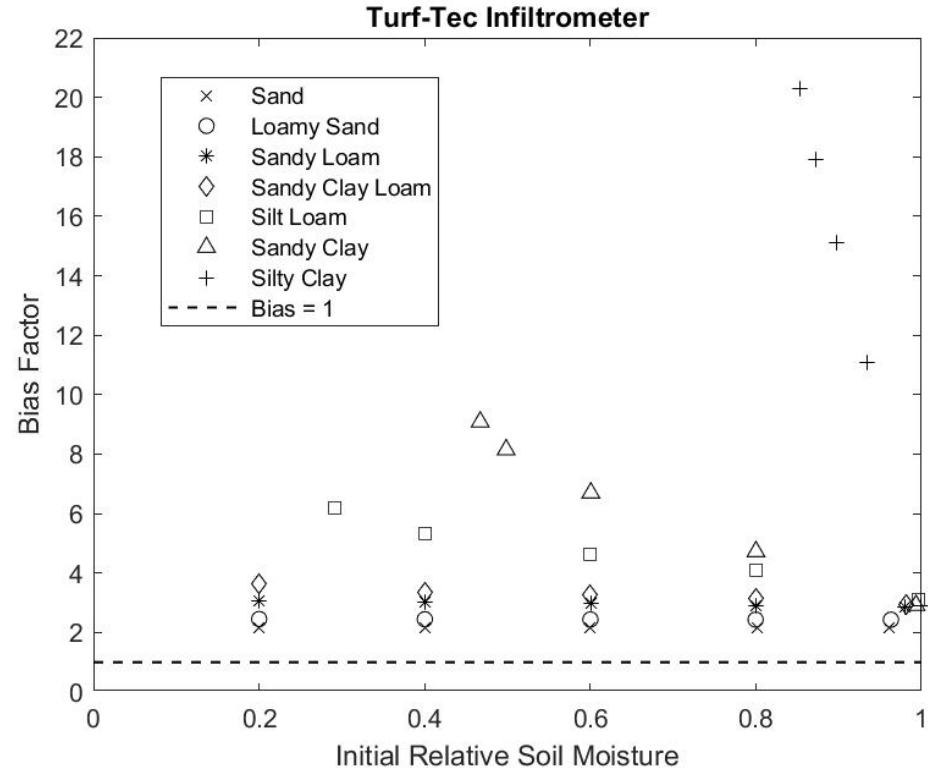
Loamy Sand at 40% Initial Relative Soil Moisture



$$\text{Bias Factor} = \frac{\text{Simulated Infiltration Rate}}{\text{Input } K_{sat}}$$

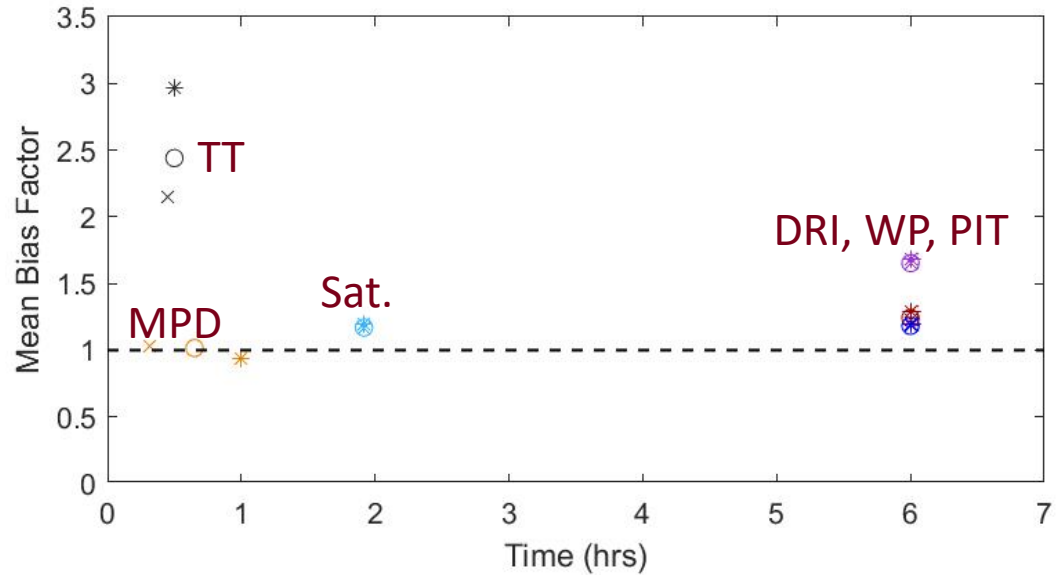
Likely sources of bias:

- For methods like TT that assume 1-D flow, lateral divergence violates assumption
- For methods that assume 3-D flow, flow approximations may not reflect actual flow pattern



Coarse Soils Typical of Infiltrating Green Stormwater Infrastructure

Soil	DRI	Sat.	WP	MPD	PIT	TT
S	×	×	×	×	×	×
LS	○	○	○	○	○	○
SL	*	*	*	*	*	*



Questions or
Comments?
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