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THE TRANSIENT MODELING OF BUBBLE PINCH-OFF USING AN ALE MOVING MESH

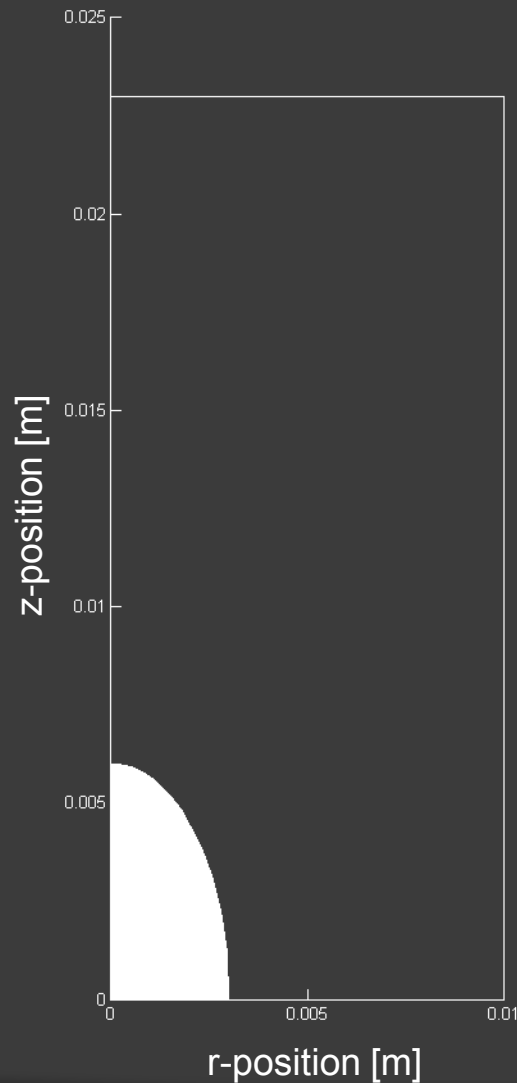
Outline

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- Level-Set and Phase-Field Comparisons
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Motivation

- ◎ This model is being developed for modeling boiling heat transfer in the presence of an acoustic field.
 - Increase critical heat flux by delaying transition to film boiling.
- ◎ Begin with modeling a single isothermal bubble going through pinch-off.

Initial Configuration



- Model is 2D axisymmetric.
- Initial geometry is used in ALE, level-set, and phase-field models.
- Initial bubble volume is $1.131e-7 \text{ m}^3$.

<u>Boundary Number</u>	<u>Type</u>	<u>Condition Satisfied</u>
1	Wall	No Penetration, Slip
2	Wall	No Penetration, Slip
3	Wall	No Penetration, Slip
4	Open Boundary	Zero Gage Pressure
5	Symmetry	Axial Symmetry
6	Symmetry	Axial Symmetry
7 (inside)	General Stress	Pressure, Continuity of Shear Stress
7 (outside)	Moving Wall	No Slip at Fluid Interface

Governing Equations

Normal-stress boundary condition: $\left(\underline{\underline{\sigma}}_l - \underline{\underline{\sigma}}_g\right) \hat{n} = \sigma \kappa \hat{n}$

Stress tensor and curvature defined as:

$$\underline{\underline{\sigma}}_{g,l} = \left[-P \underline{\underline{I}} + \eta \left(\nabla \underline{u} + (\nabla \underline{u})^T \right) \right]_{g,l} \quad \text{and} \quad \kappa = \nabla_s \cdot \hat{n}$$

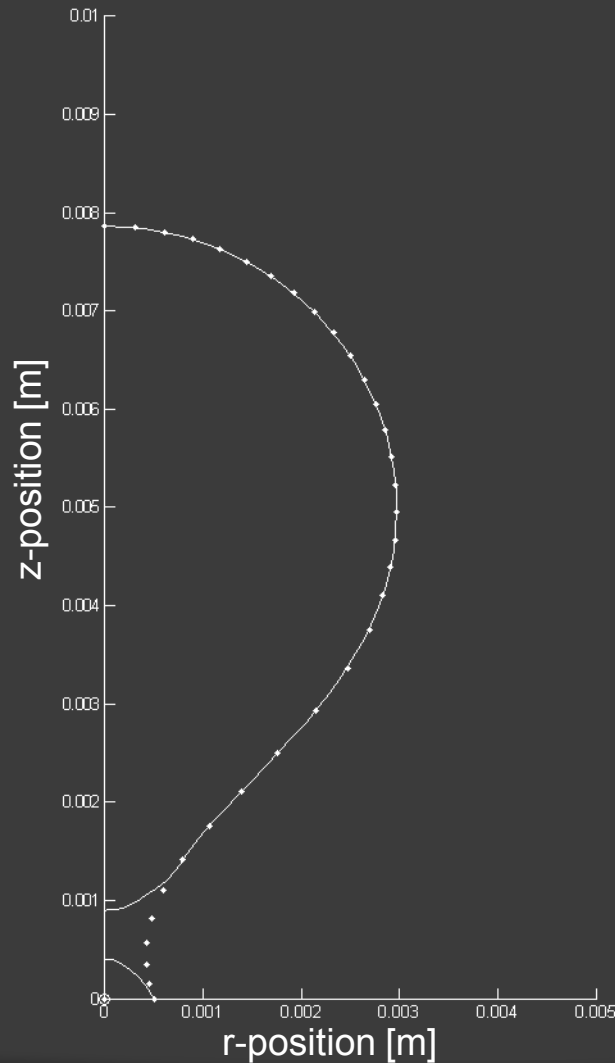
Multiplying both sides by a test function and integrating results in:

$$\int_{\partial\Omega} \left(\tilde{\varphi} \underline{\underline{\sigma}}_l \hat{n} \right) dA = \int_{\partial\Omega} \left(\tilde{\varphi} \underline{\underline{\sigma}}_g \hat{n} \right) dA + \int_{\partial\Omega} \left(\tilde{\varphi} \sigma \kappa \hat{n} \right) dA$$

Applying the surface divergence theorem and substituting back in yields:

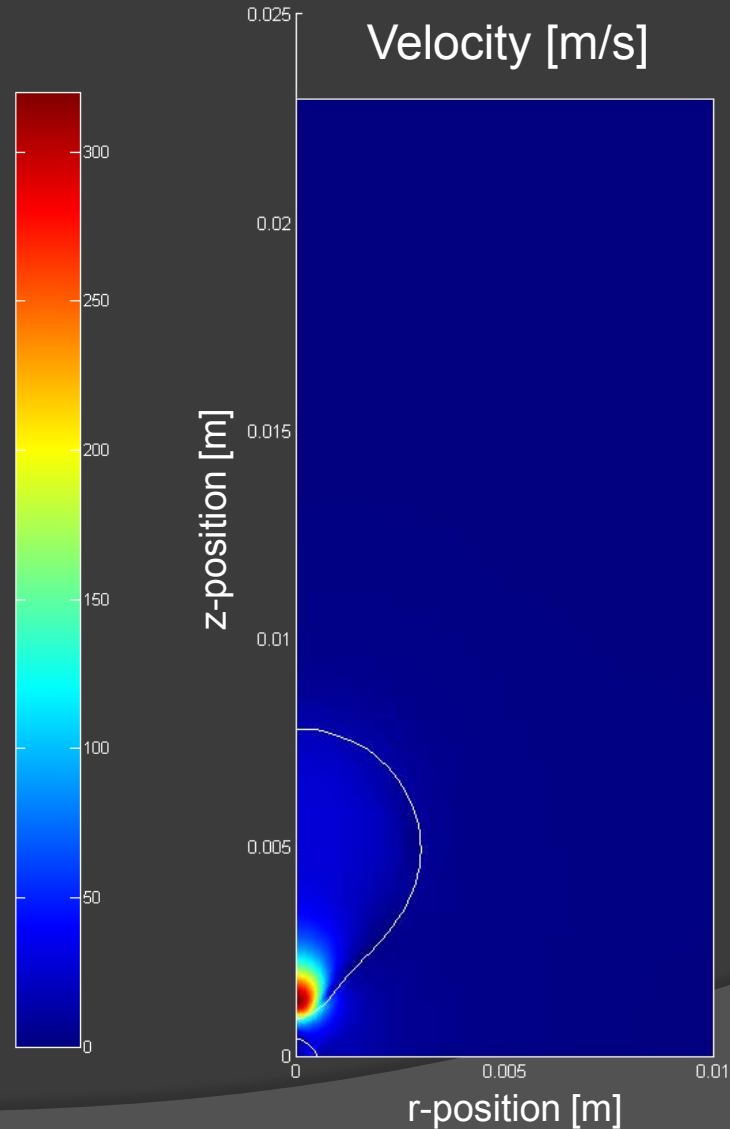
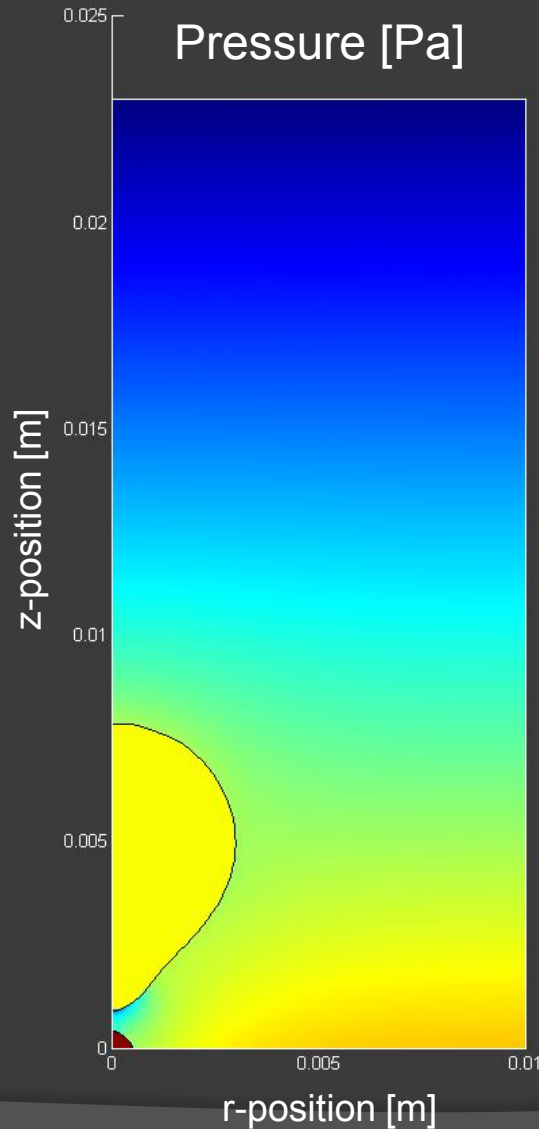
$$\int_{\partial\Omega} \left(\tilde{\varphi} \underline{\underline{\sigma}}_l \hat{n} \right) dA = \int_{\partial\Omega} \left(\tilde{\varphi} \underline{\underline{\sigma}}_g \hat{n} \right) dA - \int_{\partial\Omega} \left(\sigma \nabla_s \tilde{\varphi} \right) dA + \int_{\partial^2\Omega} \left(\sigma \tilde{\varphi} \hat{m} \right) ds$$

Pinch-Off Procedure



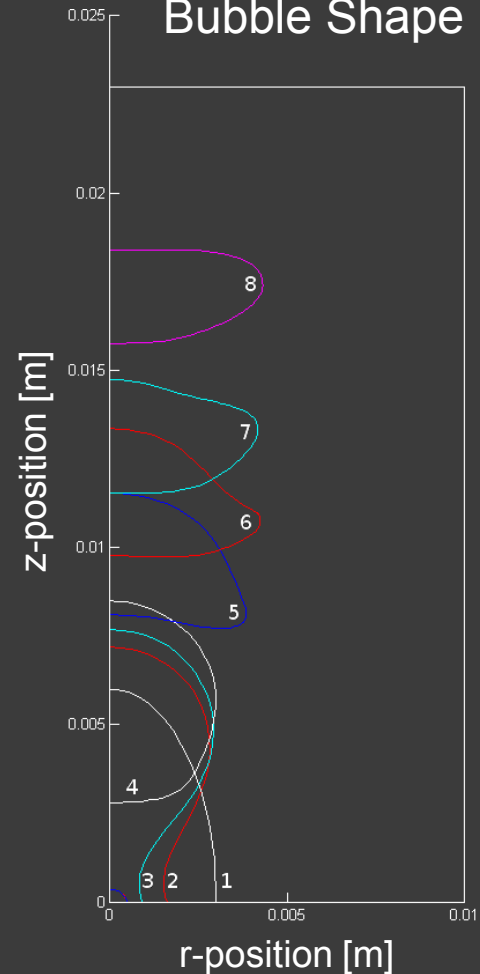
- A pinch-off point is determined visually, near the minimum neck radius. A gap height is chosen and a point is inserted at the top and bottom. Additional points are removed near the edge of the gap to get a smooth profile. Finally, the new set of points are fit with splines.
- A minimum number of points were removed to preserve as much of the original shape as possible.
- The pinch-off method in the model presented does not conserve mass during the transition.

Pinch-Off Procedure (cont.)

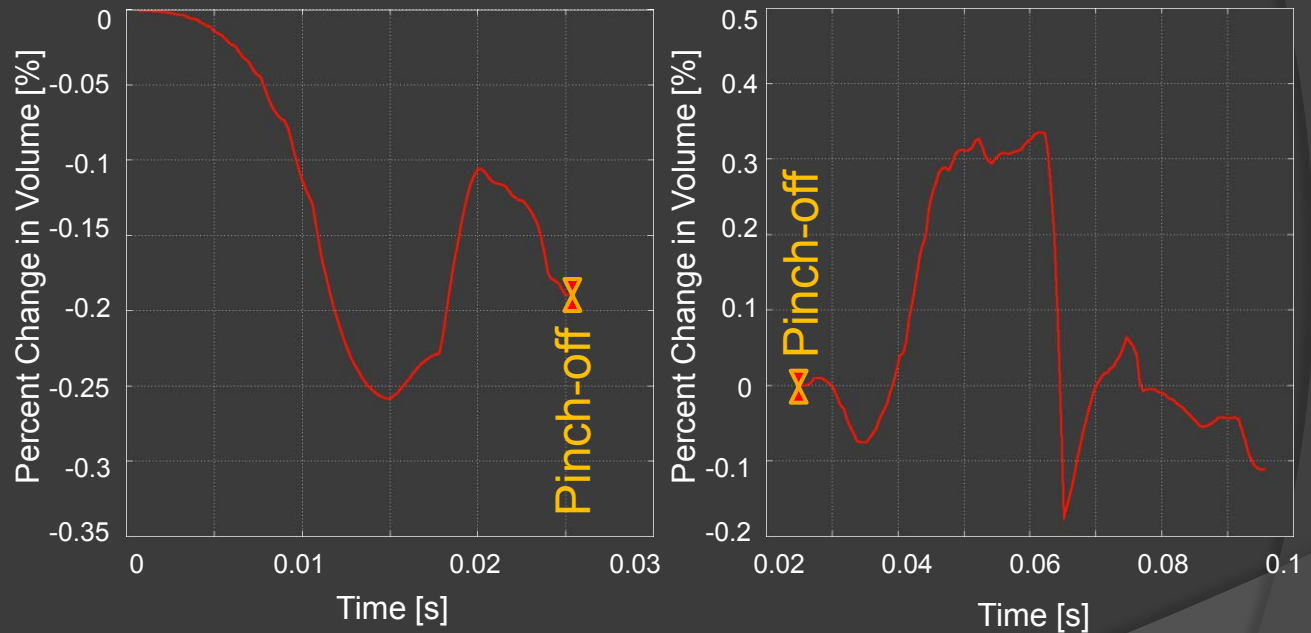


ALE Simulation Results

Bubble Shape Evolution

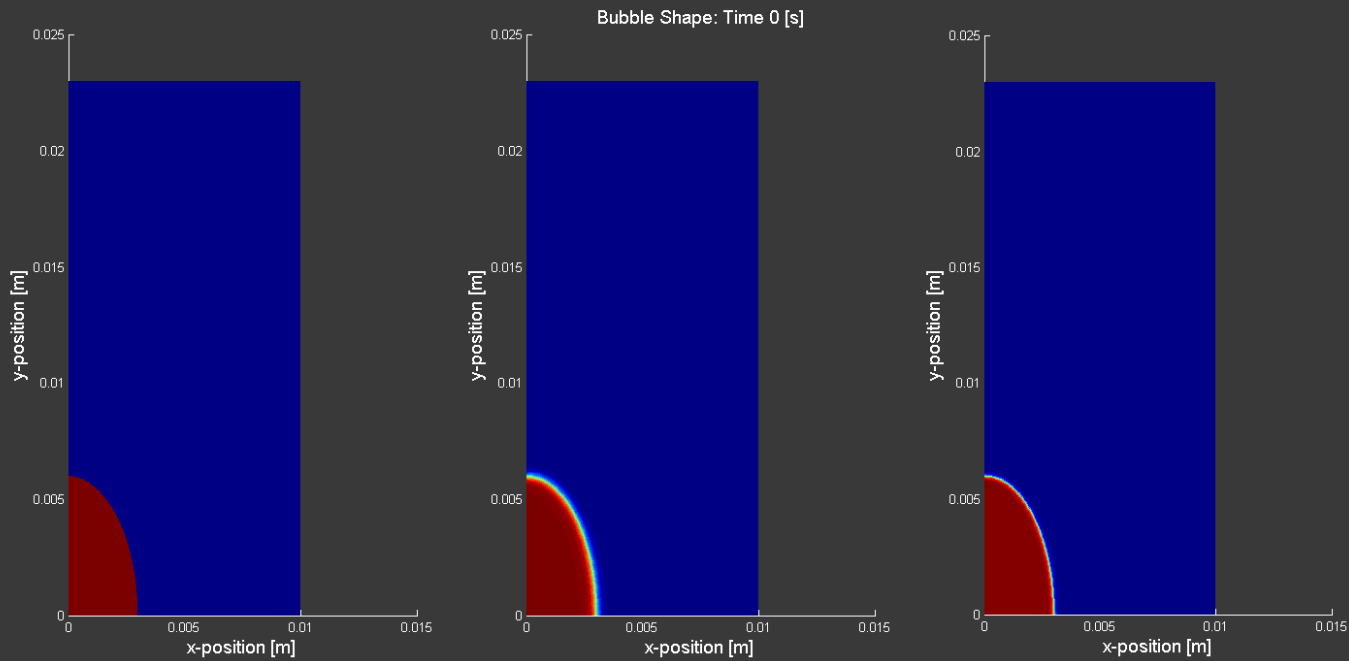


Mass Conservation



Rel. Tolerance – 0.01
Abs. Tolerance – 0.001

Level-Set and Phase-Field Comparisons



ALE
(Slip BC)

Level-Set
(Slip Length BC)

Non-Conservative
Phase-Field
(No-Slip BC)

Level-Set and Phase-Field Comparisons (2)

<u>Model Type</u>	<u>Solution Time [min]</u>	<u>Simulation End Time [s]</u>	<u>t^* [min/ms]</u>
ALE	30	0.096	0.31
LS	700	0.069	10.1
PF Conserv.	280	0.050	5.6
PF, Non-Conserv.	105	0.100	1.05

<u>Model Type</u>	<u>Peak Memory Usage [GB]</u>
ALE	4
LS	4.5
PF, Non-Conserv.	7

$$t^* = \frac{(\text{Computation Time})}{(\text{Simulation Duration})}$$

Conclusions

ALE method:

- Provides a sharp interface to apply boundary conditions.
- Tracks fluid interface and conserves mass well.
- Reduces computing requirements in both CPU capabilities and memory capacity.
- ALE application mode allows for the use of a contact line with a fixed angle and no-slip, slip-length parameter, or slip conditions.
- Alternatively, a fixed contact line can be enforced while allowing change in contact angle.

Future Work

- ⦿ The pinch-off process will be modeled using asymptotic approximations to compute the new geometry immediately after pinch-off and the corresponding velocity and pressure fields.
 - The spatial and time scales become too small to numerically resolve in a reasonable time frame.
- ⦿ Incorporate heat transfer and pressure acoustic application modes.

Questions?

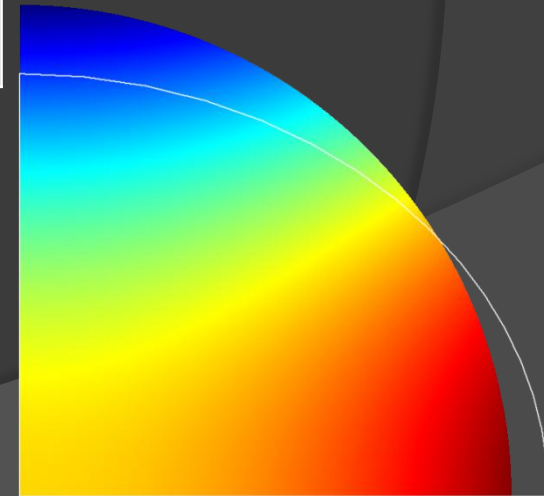
Tolerances – Study

Percent Change in Mass

	0.01	0.005	0.001	0.0005	0.0001	Rel. Tol.
0.001	0.7778	0.6748				
0.0005		0.4670	0.1724			
0.0001			0.0396	0.0202		
0.00005				-0.01		
0.00001					-0.0147	

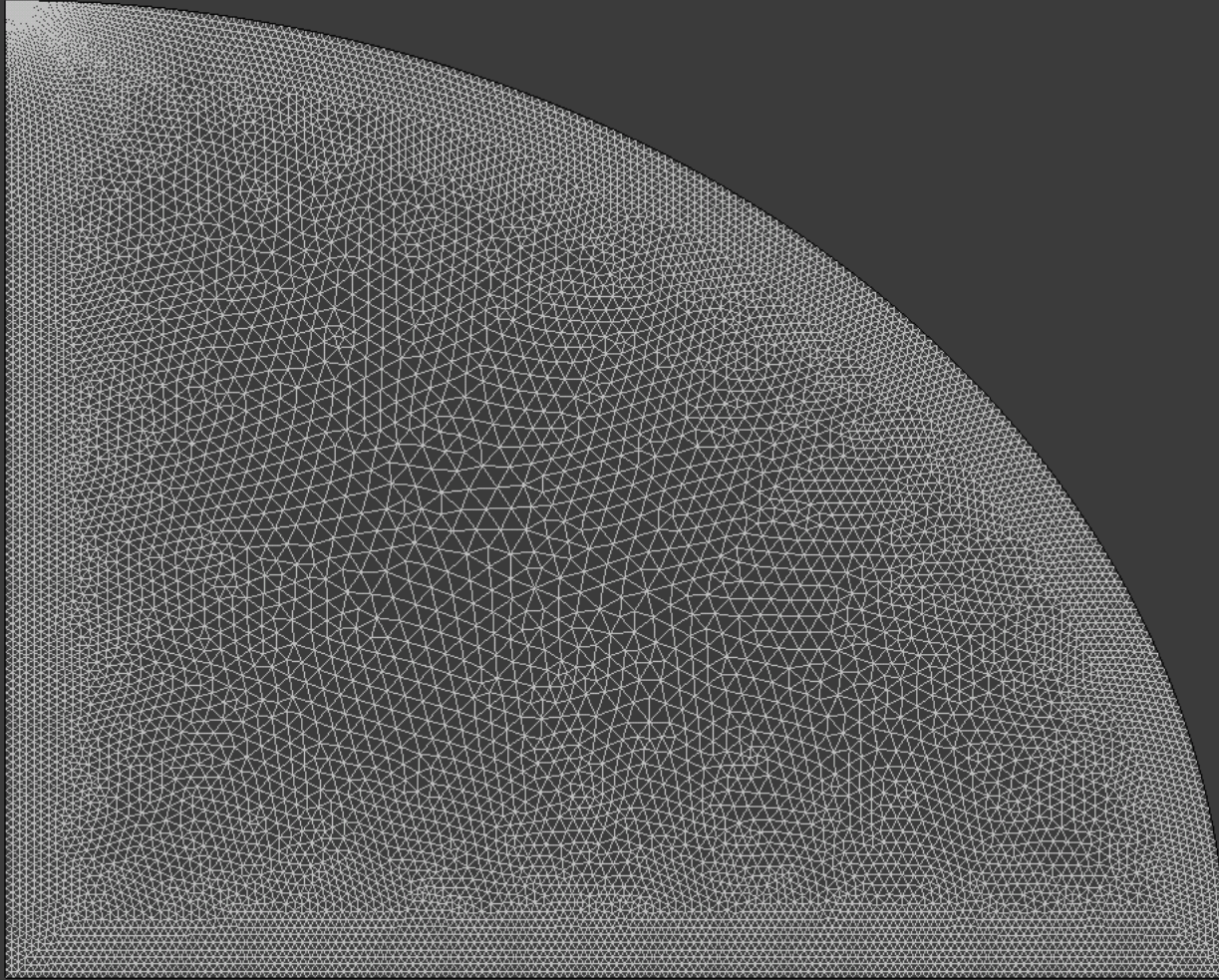
Abs. Tol.

$R_o = 3\text{mm}$



$R_o = 3.75\text{mm}$

Tolerances – Study (2)



Level-Set and Phase-Field Boundary Conditions

Boundary Settings - Two-Phase Flow, Laminar, Level Set (chns)

Equation

$$\mathbf{n} \cdot \mathbf{u} = 0, \mathbf{t} \cdot [-p\mathbf{I} + \eta(\nabla\mathbf{u} + (\nabla\mathbf{u})^T)]\mathbf{n} = 0$$

$$\mathbf{F}_{\text{fr}} = -(\eta/\beta)\mathbf{u}, \mathbf{n} \cdot \mathbf{n}_{\text{interface}} = \cos(\theta)$$

Boundaries Groups

Boundary selection

Group:

Select by group

Interior boundaries

Coefficients Color/Style

Boundary conditions

Boundary type: Wall

Boundary condition: Wetted wall

Quantity	Value/Expression	Unit	Description
θ	theta*pi/180	rad	Contact angle
β	h	m	Slip length

OK Cancel Apply Help

Boundary Settings - Two-Phase Flow, Laminar, Phase Field (chns)

Equation

$$\mathbf{u} = 0$$

$$\mathbf{n} \cdot \epsilon^2 \nabla \phi = \epsilon^2 \tan(n/2 - \theta_w) |\nabla \phi - (\mathbf{n} \cdot \nabla \phi) \mathbf{n}|$$

$$\mathbf{n} \cdot (\gamma/\epsilon^2) \nabla \psi = 0$$

Boundaries Groups

Boundary selection

Group:

Select by group

Interior boundaries

Coefficients Color/Style

Boundary conditions

Boundary type: Wall

Boundary condition: Wetted wall

Quantity	Value/Expression	Unit	Description
θ_w	theta*pi/180	rad	Contact angle

OK Cancel Apply Help

Pre-Pinch-Off Pressure and Velocity Fields

