



# Numerical Simulation of Flow Electrolysers: Effect of Various Geometric Parameters



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# Outline

- Electrolysis and its Industrial applications
- Objective of this work
- Governing equations and boundary conditions
- Validation of the computational approach
- Effect of inlet channel length
- Effect of offset between anode and cathode
- Effect of size of anode
- Conclusion

### **Electrolysis and its Industrial Applications**



### **Objective of this Work**



Li Lianhua, Kong Xiaoying, Sun Yongming, Yuan Zhenhong, Li Ying, Performance of microbial fuel cell in different anode and cathode sizes, *International Conference on Remote Sensing, Environment and Transportation Engineering*, 7707-7710 (2011)

### **How We Proceed**

Applicable governing equations and boundary conditions. Validation of computational approach Effect of geometrical parameters (inlet channel length, offset, anode length) on potential

#### Conclusions

### **Governing Equations and Boundary Cond.**

**Navier- Stokes Equations** 

$$\nabla \bullet \mathbf{u} = 0 \qquad \rho \mathbf{u} \bullet \nabla \mathbf{u} = \mu \nabla^2 \mathbf{u} - \nabla p + \rho \mathbf{g}$$

**Nernst-Planck equations** 



#### Possible boundary conditions for NP equations

Current/potential BC		<b>Concentration BC</b>	
<i>n</i> . <i>i</i> = 0	(Electrical insulation)	$C = C_o$ (0	Constant concentration)
$i = i_0$	(Constant inward current density )	$-\bar{n}.\bar{N_{\iota}}=i_{o}/F$	(Constant flux)
$i = -i_0$	(Constant outward current density)	$-\overline{n}.\overline{N}_{t}=0$	(Zero flux)
$v = v_o$	(Constant potential)	$-\bar{n}.\left(-D_i\nabla C_i - \frac{z_iF}{RT}D_iC_i\nabla\emptyset\right) = 0$	(Convective flux)

### **Governing Equations and Boundary Cond.**



Wall	Current potential boundary cond.		Concentration/flux boundary cond.	
1	Insulation	$\mathbf{n} \bullet \mathbf{i} = 0$	Concentration	$c_2 = c_o$
2	Insulation	$\mathbf{n} \bullet \mathbf{i} = 0$	Zero flux	$-\mathbf{n} \bullet \mathbf{N}_2 = 0$
3	Insulation	$\mathbf{n} \bullet \mathbf{i} = 0$	Zero flux	$-\mathbf{n} \bullet \mathbf{N}_2 = 0$
4	Current density	$\mathbf{i} = i_o$	Faraday's law	$-\mathbf{n} \bullet \mathbf{N}_2 = \pm \frac{i_0}{F}$
5	Voltage	$V = V_o$	Zero flux	$-\mathbf{n} \bullet \mathbf{N}_2 = 0$
6	Insulation	$\mathbf{n} \bullet \mathbf{i} = 0$	Convective flux	$-\mathbf{n} \bullet (-D_2 \nabla c_2) - z_2 u_{mi2} F c_2 \nabla V) = 0$

### Validation of the Computational Approach





Concentration profile of species 1 at the outlet for  $i_o$ =10000A/m<sup>2</sup>,  $u_o$  = 0.01m/s,  $c_o$ =600mol/m<sup>3</sup>

[1] Jun Lu, Dong-Jie Li, Li-Li Zhang, Yu-Xin Wang (2007). Numerical simulation of salt water electrolysis in parallel plate electrode channel under forced convection. Electrochimica Acta, 53 : 768–776.)

[2] Pragati Shukla, K.K. Singh, P.K. Tewari, P.K. Gupta (2012). Numerical simulation of flow electrolysers: Effect of obstacles, Electrochimica Acta, **79**, 57–66)

### Validation of the Computational Approach



Concentration profile of species 1 at the outlet for  $u_o = 0.05 \text{ m/s}$ ,  $i_o = 10000 \text{ A/m}^2$ ,  $c_o = 600 \text{ mol/m}^3$ 



Potential profile at the outlet for  $u_o = 0.01$  m/s,  $i_o = 10000$ A/m<sup>2</sup>,  $c_o = 600$  mol/m3



Velocity vector and velocity contours for geometries G-1 to G-2

#### Comparison of geometries with and without inlet channels

Geometry	Current density for constant applied voltage		
	J (A/m²)		
G-1	6729.16		
G-2	7067.30		

Pragati Shukla, K.K. Singh, P.K. Tewari, P.K. Gupta, Numerical simulation of flow electrolysers: Effect of obstacles, Electrochimica Acta, **79**, 57–66 (2012)



Range of parameters-Two charged species- (Na+ and Cl)

4Current density- (2000 -10,000A/m<sup>2</sup>)

Base case- No inlet channel.

Inlet length-( 20% to 100%)
of electrode length)

Inlet flow velocity -0.03
m/s

Initial electrolyte concentration -600 mol/m<sup>3</sup>





### **Effect of Offset between Anode and Cathode**



Effect of providing offset between the location of anode and cathode at current density 10,000  $A/m^2$ 

↓anode length 20 cm and cathode length 50 cm.

No inlet channel

As expected, as the offset increases the potential difference across the electrode increases for a given current density.

↓It is therefore better to design an electolyser in which anode and cathode are of different length such that the offset between the anode and cathode is kept minimum.

### **Effect of Size of Anode**



Effect of varying anode length on potential difference at current at current 2000 A

Constant total current 2000A.

The offset between the anode and cathode is zero for these simulations.

As the length of anode reduces, the potential difference between the electrode increases

### **Effect of Size of Anode**

Surface normalized potential and current density vector plots for anode of 50 cm lengths at current 2000 A

Surface normalized potential and current density vector plots for anode of 10cm lengths at current 2000 A

Min: 5.597e-9

### Conclusions

- The simulations reported in this work provide useful insights into how the performance of a flow electrolyser is affected when certain geometric parameters namely inlet channel length, offset between anode and cathode and the length of anode are changed.
- The results also show that providing an inlet channel having length about 20-30% of electrode length improves the performance of electroneutral bulk.
- Results show that providing offset, increases the potential drop for same applied current and hence leads to inefficient electroneutral bulk.
- Simulations also show that as length of one of the electrode reduces, keeping the current same, performance of electroneutral bulk degrades.
- These multiphysics simulations also highlight that it is important to consider both Nernst -Planck and Navier Stokes equations while simulating electroneutral bulk of a flow electrolyser.

# THANKS FOR YOUR ATTENTION!

# **QUESTIONS, COMMENTS?**